



Orbital Angular Momentum Optical Amplifier Based on PbS-Doped Ring-Core Fiber

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A unique orbital angular momentum (OAM) optical amplifier based on a ring-core fiber doped with lead sulfide (PbS) is realized for the first time in this study. The PbS-doped ring-core fiber is fabricated using the modified chemical vapor deposition method. The cross-sectional microscope image of the fiber is obtained. The difference in the refractive index between the ring core and the fiber cladding measured by a three-dimensional refractive index tester reaches 1%. The sulfur and lead content in the ring-core of the PbS-doped ring-core fiber is confirmed by energy spectrum analysis. A first-order OAM optical amplifier is built based on the PbS-doped ring-core fiber. The experiment confirms that the air-hole PbS-doped ring-core fiber can support the OAM $|l| = 1$ modes. In addition, 2.3 dB of on-off gain is obtained for the OAM $|l| = 1$ modes at 1,550 nm. The fluorescence spectrum obtained using the backward pumping method ranges from 1,100 to 1,600 nm.

Keywords: optical fiber amplifier, PbS-doped ring-core fiber, orbital angular momentum (OAM), on-off gain, fluorescence properties

INTRODUCTION

Mode division multiplexing (MDM) can be used to considerably expand the capacity of optical communications by using orthogonal modes to transmit signals [1, 2]. In 2004, a new MDM communication scheme based on the photon orbital angular momentum (OAM) was proposed [3]. The initial studies had focused on the transmission of OAM modes in free space and suffered from short transmission distances. Since 2009, the index separation between adjacent OAM vector modes has been considerably enhanced by ring-core optical fiber structures [4–10]. In 2013, Bozinovic et al. [11] implemented OAM mode multiplexing in a ring-core optical fiber with a length of more than 1.1 km. This shows that OAM can provide additional options for data multiplexing in future fiber optic networks. A variety of OAM amplifiers based on erbium-doped fibers have been theoretically designed [12–14] to address the unavoidable signal-transmission loss in long-distance communications. In the year 2017, Jung et al. [15] built the air-hole erbium-doped fiber amplifier (EDFA) to amplify the OAM $|l| = 1$ modes for the first time. The gain of the OAM $|l| = 1$ modes with a cladding pump was up to 15.7 dB for the wavelength ranging from 1,545 to 1,600 nm. Xing et al. [16] used the erbium-doped few-mode fiber to build the all-fiber amplifier and realized the first-order OAM mode amplification in the year 2018, and the gain was 37.2 dB.

However, the bandwidth of EDFA cannot cover the entire communication band of the OH-free silica fiber. Therefore, an alternative active material is proposed for optical fiber amplifiers [17–19].

Because lead-sulfide (PbS) quantum dots have strong quantum-confined effects, the luminescence center of PbS quantum dots ranges from 1,000 to 1,800 nm, which is sufficient to realize the tunable photoluminescence in the near-infrared [20, 21]. PbS nanomaterials have great application prospects in optical amplifiers, lasers [22, 23], and sensors. The optical-gain performance has been observed in a glass medium doped using PbS quantum dots [24, 25]. The amplification in PbS quantum dot-doped fibers in common communication bands has been considerably enhanced through improvements in various PbS-based doping methods [26–30]. In the year 2018, Huang et al. [31] presented a new method, named “melt-in-tube,” for preparing PbS quantum dot doped fiber. The PbS quantum dots with diameters from 1.0 to 5.0 nm were uniformly precipitated in the PbS quantum-dots doped glass fiber core. However, the fiber loss was considerable, i.e., >14 dB/m.

In this study, we realize the amplification of the first-order OAM, which is based on an air-hole PbS-doped ring-core fiber. The fiber is fabricated using the modified chemical vapor deposition (MCVD) technology. The fluorescence spectrum ranges from 1,100 to 1,600 nm. Under the pumping of a 980 nm laser, the on-off gain (up to 2.3 dB) of the OAM $|l| = 1$ modes with a signal light at 1,550 nm could be achieved.

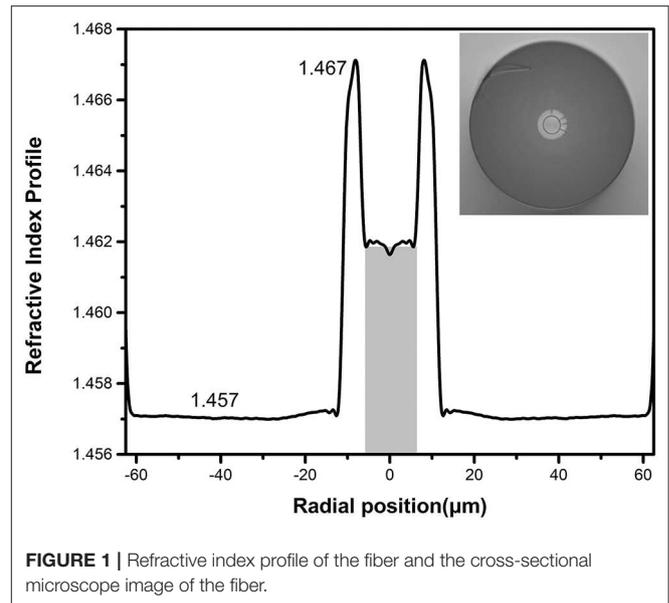
DESIGN AND FABRICATION OF AIR-HOLE PBS-DOPED FIBER

Preparation of Optical Fiber

A considerable number of studies and experiments have shown that the effective index separation of OAM modes should be $>10^{-4}$ to support OAM mode transmission in the long haul. This can be realized by introducing a high index ring into the traditional fiber structure [5].

In this study, PbS powder is doped into the ring core of the fiber to support the transmission and amplification of OAM modes. An air-hole ring-core fiber doped using PbS is fabricated via MCVD. The process involved the following steps: First, SiCl_4 and GeCl_4 are carried by high-purity oxygen into a silica substrate tube, along with PbS, which is vaporized by high-temperature heating. Second, the porous soot layer is deposited on the inner surface of the substrate tube. Third, at a high temperature of $2,000^\circ\text{C}$, the silica substrate tube is disposed via a vitrification process and collapsed into a PbS-doped optical fiber preform. Finally, the preform is drawn into an air-hole PbS-doped ring-core fiber with certain geometric parameters by using a drawing tower. During the drawing process, the structural parameters of the optical fiber can be controlled by the temperature of drawing, the preform feeding speed and the drawing speed.

The cross-sectional image of the fabricated fiber is observed via optical microscopy, and the refractive index profile of the fiber can be measured using a three-dimensional refractive-index tester (Model: SHR-1602, Shanghai University, China). As depicted in **Figure 1**, the interior of the ring has a diameter of $9.80\ \mu\text{m}$ and is filled with air. The external diameter of the ring is $20.49\ \mu\text{m}$, and the thickness of the ring is $5.35\ \mu\text{m}$. In addition,



the diameter of the cladding is $130.22\ \mu\text{m}$. The refractive-index difference between the ring and cladding of the fiber reaches 1% (the gray part in **Figure 1** represents the air hole filled using index-matching oil). The total length of the sample fiber is about 60 m. The loss of the fiber at 1,500–1,570 nm is about 19 dB.

Mode Simulation

The RF module of COMSOL software is used to simulate the waveguide mode of optical fiber. The amplitude of the field decays rapidly as a function of the cladding radius. The cladding radius of the sample fiber is large enough for the field of the confined modes to reach zero at the exterior boundaries. This constitutes a valid boundary condition. Parameters such as the refractive index, cladding radius, ring core radius, and air hole radius of the sample optical fiber are set in the simulation. In addition, we use triangular grids to divide each part of the optical fiber. The region of air hole, ring core and cladding are divided into 148, 230, and 2,028 grids, respectively. Thus, the HE_{11} , TE_{01} , TM_{01} , HE_{21} , HE_{31} , EH_{11} , HE_{51} , and EH_{31} vector modes transmitted by the fabricated PbS-doped ring-core fiber can be analyzed using the COMSOL software. The effective indexes of the modes are listed in **Table 1**. The effective index separation of the OAM $|l| = 1$ modes is 0.65×10^{-4} , via calculation.

CHARACTERIZATION ANALYSIS AND FLUORESCENCE SPECTRUM OF OPTICAL FIBER

Energy-spectrum analysis is used to prove that the PbS material is successfully doped in the fiber. The element content in the three points indicated on the high-index ring depicted in **Figure 2** are analyzed and the results are shown in **Table 2**. It can be seen that in each of the selected regions, there exist the elements of Si, O, C, Pb, S, and Ge, thereby indicating that PbS is successfully

TABLE 1 | Effective index.

Vector mode	Effective index
HE ₁₁	1.462554
TE ₀₁	1.462229
TM ₀₁	1.462363
HE ₂₁	1.462298
EH ₁₁	1.461539
HE ₃₁	1.461546
HE ₅₁	1.458627
EH ₃₁	1.458637

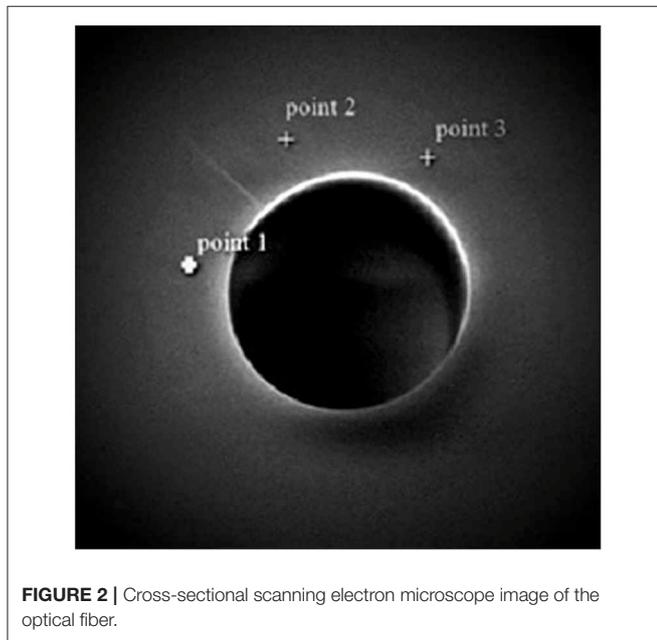


FIGURE 2 | Cross-sectional scanning electron microscope image of the optical fiber.

TABLE 2 | Element content analysis results.

Element	Point 1 (Wt%)	Point 2 (Wt%)	Point 3 (Wt%)
O	45.23	45.11	44.86
Si	43.81	43.26	43.33
Ge	10.15	10.55	10.34
Pb	0.65	0.67	1.16
S	0.16	0.41	0.31
total	100.00	100.00	100.00

doped into the air-hole ring-core fiber. However, the contents of elements Pb and S are different in different regions, indicating that the doping concentration of the PbS material is not uniform during the fiber-fabrication process.

The fluorescence spectrum of the optical fiber is measured using the backward pumping method. A 980 nm laser is selected as the pump light source. **Figure 3** shows the fluorescence spectra of the fiber measured using an optical spectrum analyzer under various pump powers ranging from 100 to 700 mW. The

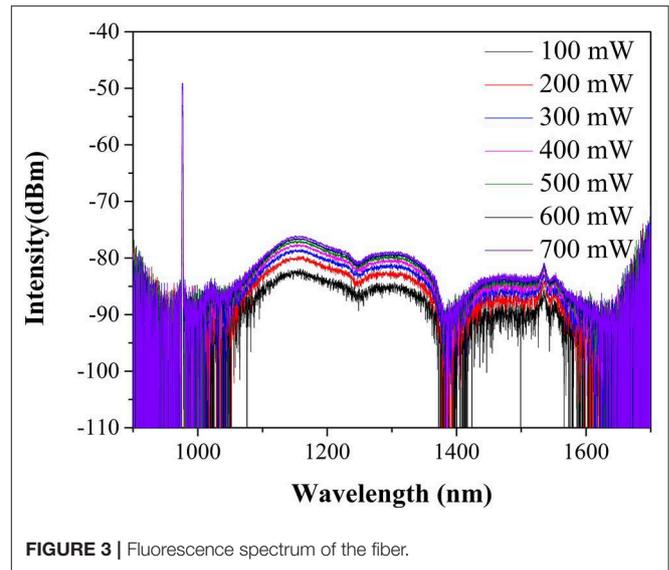


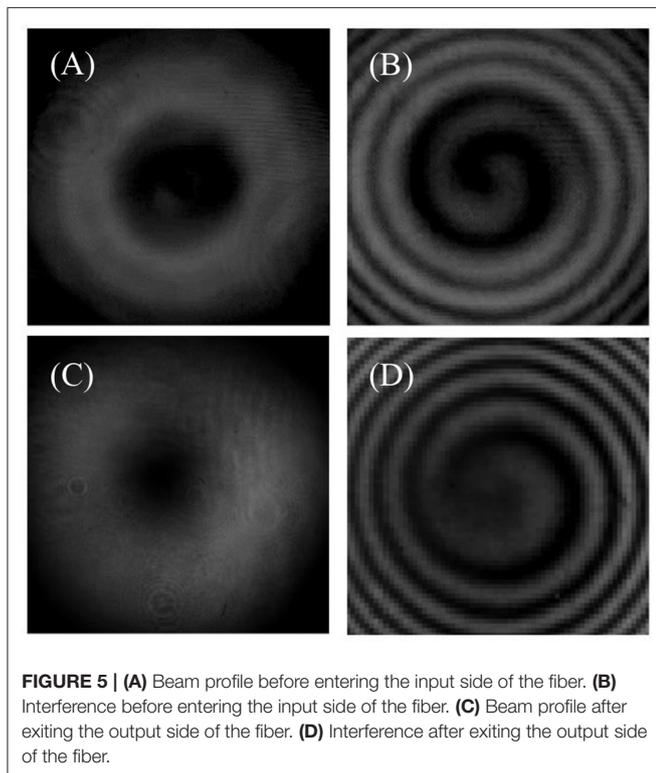
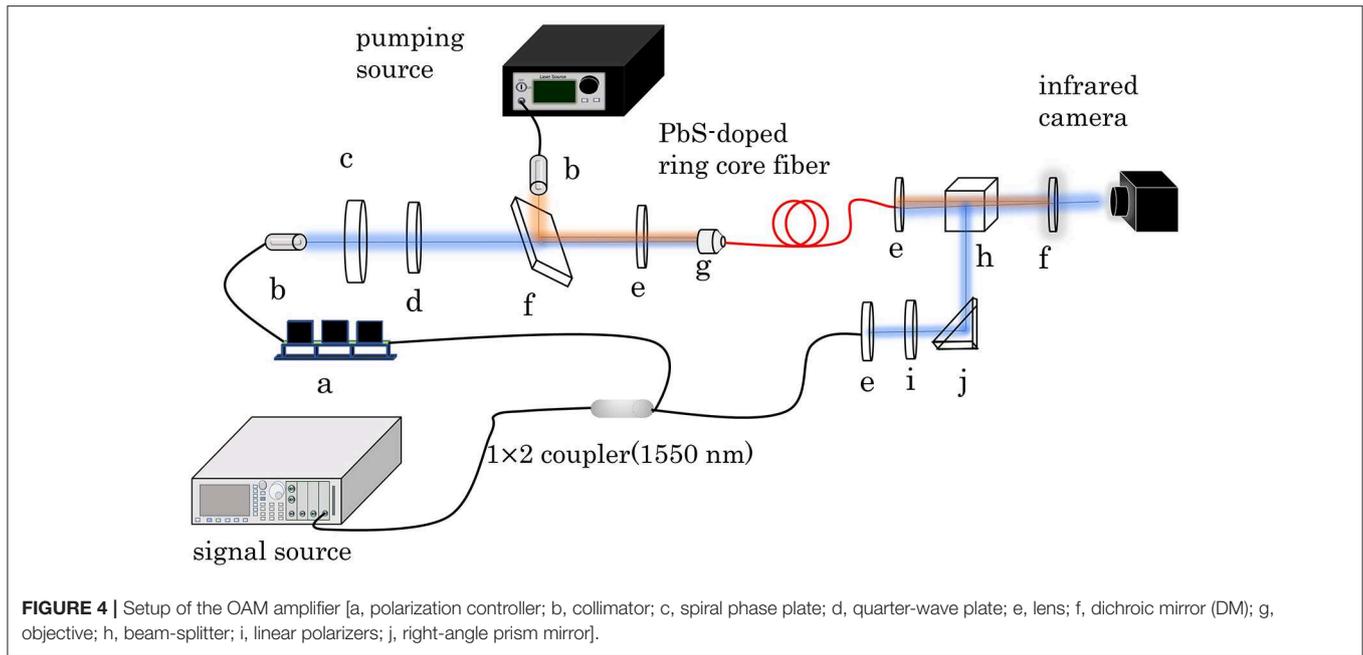
FIGURE 3 | Fluorescence spectrum of the fiber.

fluorescence spectra ranges from 1,100 to 1,600 nm. In addition, the fluorescence intensity gradually increases with the pump power. The fluorescence intensity increases by only a small amount when the pump power increases from 600 to 700 mW, and is almost unchanged and tends toward saturation when the pump power is further increased.

OAM MODE GENERATION AND AMPLIFICATION

An amplification system for the OAM $|l| = 1$ modes is built using the fabricated fiber. The experimental setup is depicted in **Figure 4**. The Gaussian signal light is split into two beams using a 1×2 coupler. The first beam serves as an interference spherical reference beam. The second beam is converted into a vortex beam using a spiral phase plate. Both the signal light and pump light are coupled into the fabricated fiber using the DM. The OAM $|l| = 1$ modes are successfully amplified subsequently. In addition, the beam profiles of the first-order vortex beam and the interference could be observed using an infrared camera. The DM before the infrared camera is used to filter out the pump light.

The beam profile of the OAM $|l| = 1$ modes before entering the optical fiber input is depicted in **Figure 5A**, and their interference pattern in **Figure 5B**. The beam profile and the interference after exiting the output side of the air-hole PbS-doped ring-core fiber are depicted in **Figures 5C,D**, respectively. The interference with the spherical reference wave in **Figure 5B** proves that the OAM $|l| = 1$ modes are successfully generated by the spiral phase plate. The beam profile maintained the form of a complete ring after exiting the output side of the fiber, as depicted in **Figure 5C**. A dextral spiral interference fringe is formed when the beam exiting the output side of the fiber interfered with the spherical reference beam, as depicted in **Figure 5D**. It indicates that the optical fiber could successfully support the $|l| = 1$ OAM modes.



The on-off gain of a fiber is defined as the ratio of the signal output to input power [32, 33]. In this paper, the signal power without the pump is taken as the input power and the signal power with the pump as the output power. The gray values measured by the near-infrared camera under different pump

powers responses the signal intensity. The same test area (the strip is depicted as a green line in **Figure 6A**) is used throughout the experiment so that the on-off gain of the optical fiber could be obtained from the gray values. To analyze the on-off gain of the ring-core PbS-doped fiber, the intensity is measured across a strip passing through the center depicted as a green line in **Figure 6A**. The intensity values gradually increased as the pump power increased from 0 to 750 mW. The on-off gains could be calculated from the intensities. The on-off gains of the OAM $|l| = 1$ modes at various pump powers are shown in **Figure 6B**. The on-off gain of the OAM₁₁ mode reaches 2.3 dB when the pump power is 750 mW. The small on-off gain of the fiber is mainly attributed to the low PbS doping concentration.

CONCLUSION

We experimentally doped the PbS into a ring-core fiber by using the MCVD method to realize the amplification of the OAM₁₁ mode. The refractive index difference between the cladding and ring core of the fiber is 1%. The fluorescence spectrum of the fiber ranges from 1,100 to 1,600 nm, which is considerably larger than that of erbium-doped fibers and indicates that the fiber can be applied in wide-band amplification systems. This fiber not only supported the transmission of the OAM₁₁ mode but also amplified the mode. The on-off gain of the OAM₁₁ reaches up to 2.3 dB at 750 mW 980 nm pumping. The experiment can be optimized in the following two aspects to extend the applicability of the fiber to higher-order OAM modes: Firstly, a spatial light modulator can be used to replace the helical phase plate, so that the order of the OAM modes generated can be adjusted by the spatial light modulator. Secondly, increasing the refractive index difference between the core and the cladding appropriately can enhance

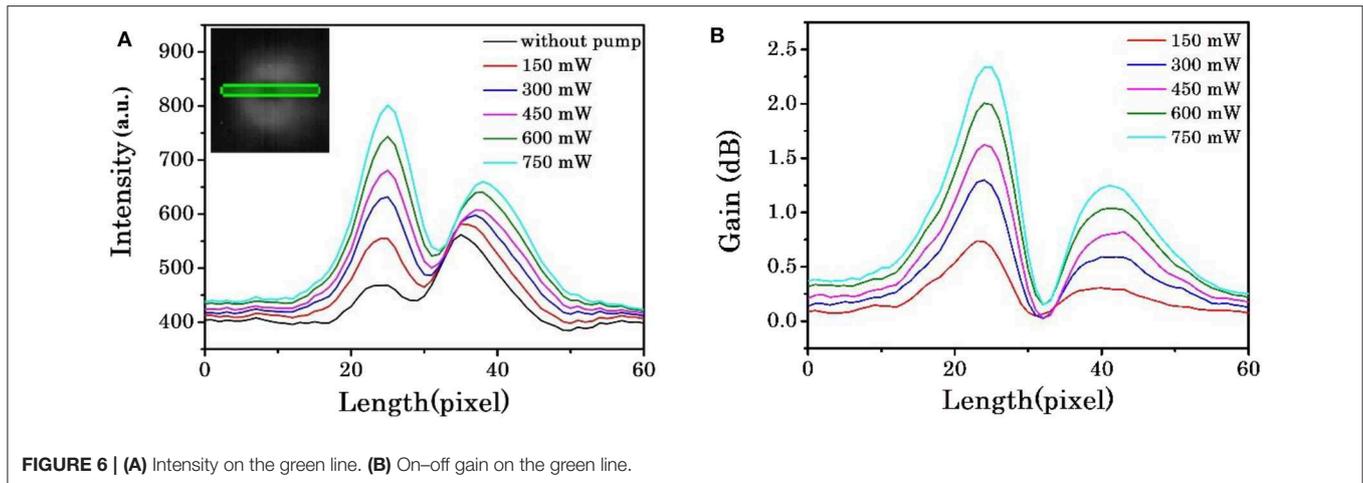


FIGURE 6 | (A) Intensity on the green line. (B) On-off gain on the green line.

the effective refractive index difference of the OAM modes and increase the number of OAM modes transmitted. In addition, the gain can be enhanced by optimizing the fiber fabrication technology to increase the PbS concentration. This type of PbS-doped ring-core optical fiber amplifier provides the possibility of realizing ultra-wideband OAM mode amplification in future all-fiber transmission systems.

DATA AVAILABILITY STATEMENT

All datasets generated for this study are included in the article/supplementary material.

AUTHOR CONTRIBUTIONS

FP and YS contributed to the conception of the study. LX contributed to conceive and design the experiments, analyzed the

data, and wrote the manuscript. LX, JY, YD, and ZC contributed to perform the experiments. HL, NC, JW, and TW helped perform the analysis with constructive discussions.

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Conflict of Interest: The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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